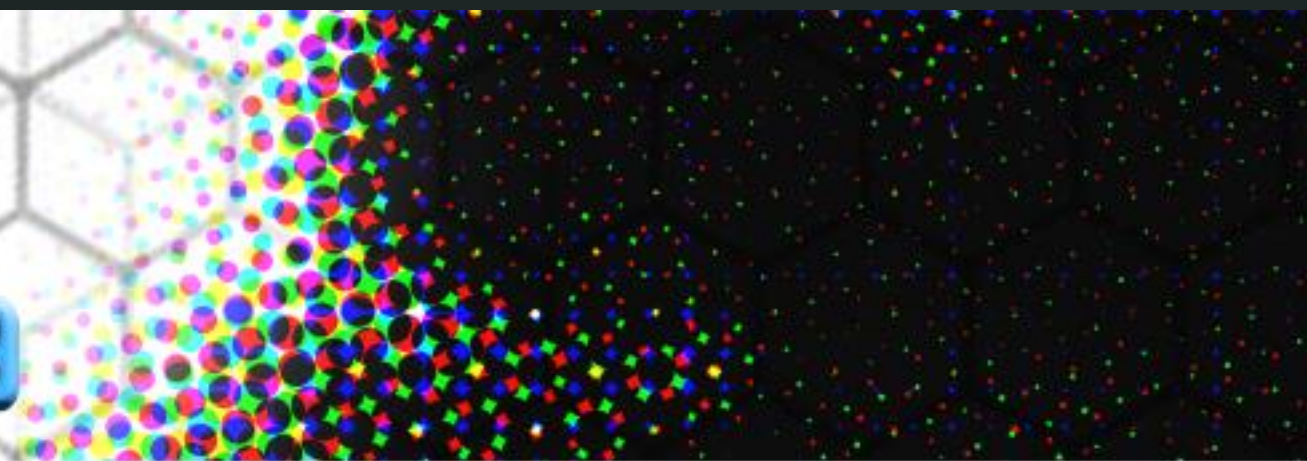


# HTS 2020 Modelling

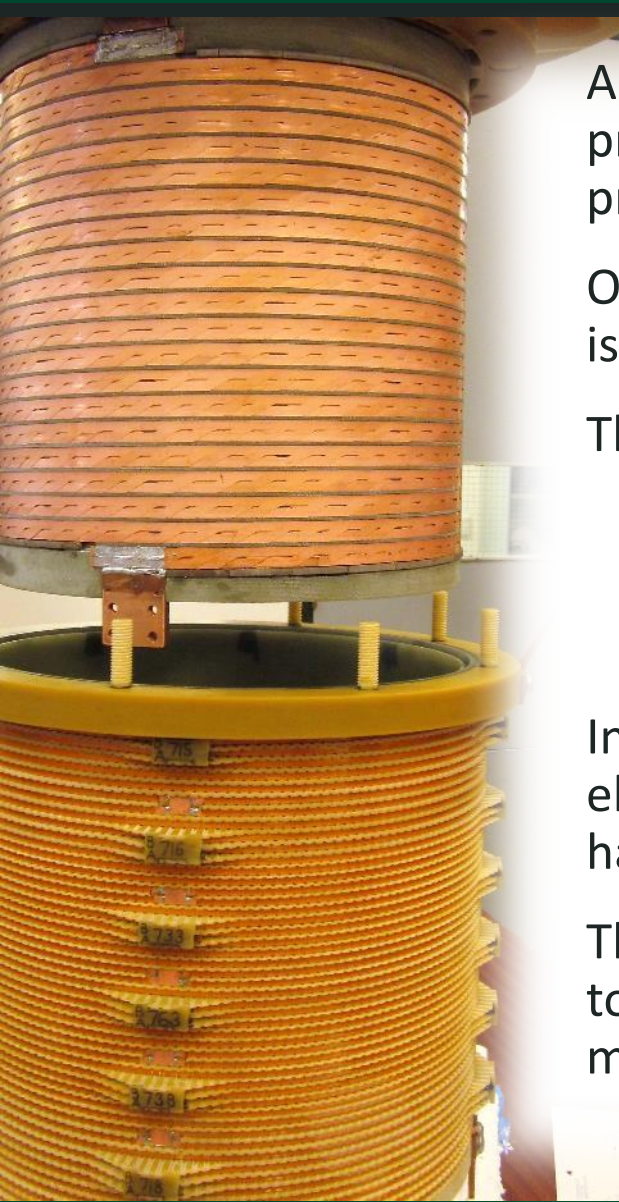


**7<sup>th</sup> International Workshop on Numerical Modelling of High Temperature Superconductors**  
22<sup>nd</sup> – 23<sup>rd</sup> June 2021, Virtual (Nancy, France)

Utilising full angle-dependent critical current data  
in the electromagnetic modelling of HTS coils

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As the construction of real-world devices from HTS coated conductors becomes more prevalent, increasingly sophisticated modelling techniques are applied to the design process.

One aspect that remains relatively rarely touched upon in practical design methodologies is the incorporation of full anisotropic critical current data in electromagnetic modelling.

This has a number of reasons:

- Scarce availability / difficulty of acquiring such data.
- Perceived difficulty of modelling such complex behaviour.
- A possible underappreciation of the variability of this data and its impact on designs.

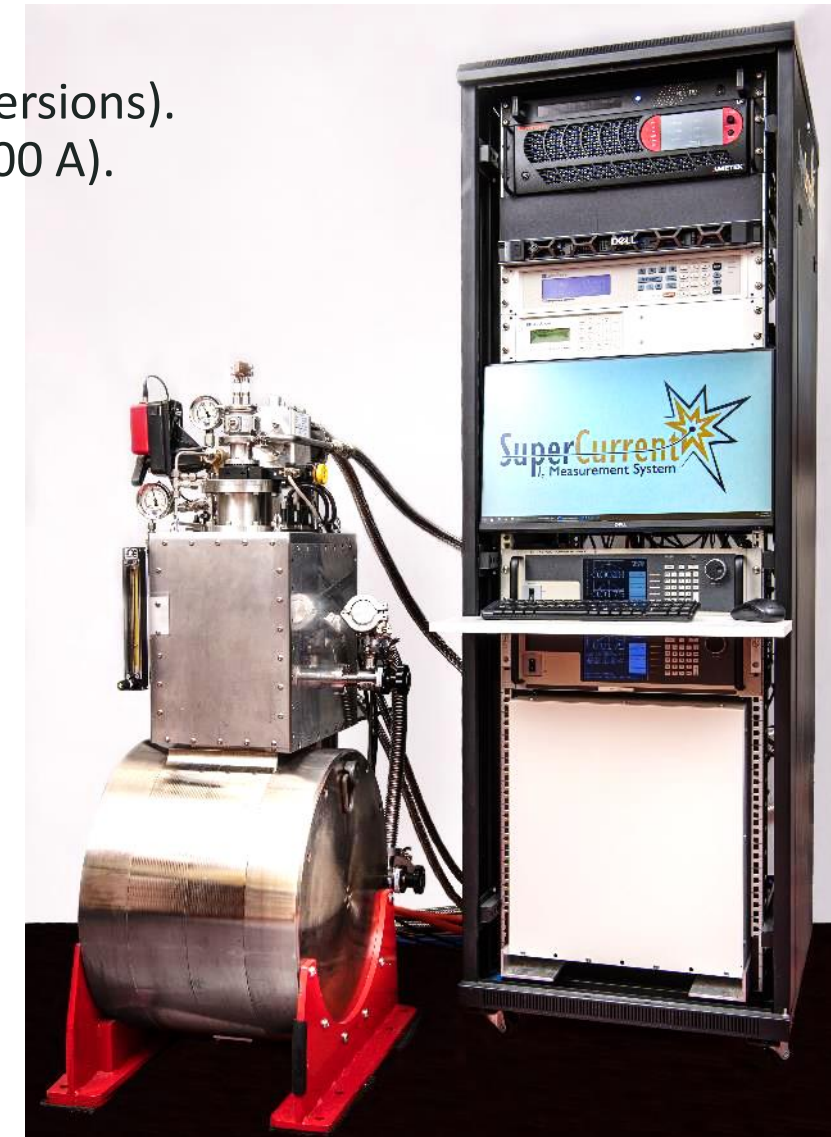
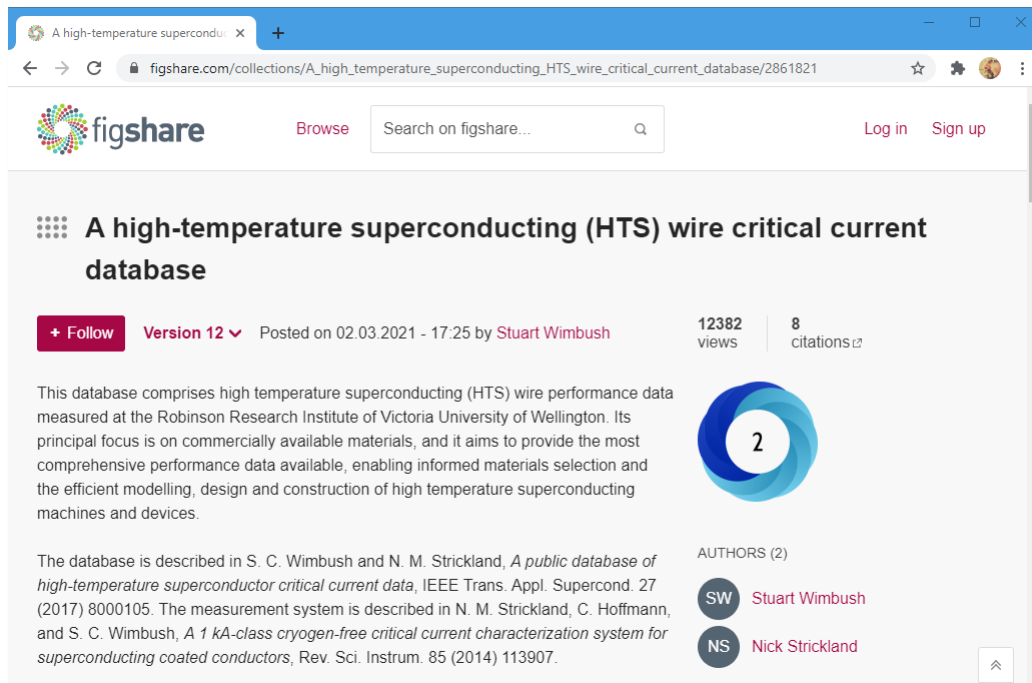
In this talk I will outline both a detailed methodology of incorporating this data into electromagnetic designs and illustrate by way of example the range of impacts it can have on the design process and the ultimate performance of the device.

The tools used here are chosen to be available to anyone who wishes to investigate this topic for themselves. The approaches outlined are applicable to any electromagnetic modelling package.



- Temperatures down to 15 K.
- Fields up to 8 T (12 T in some versions).
- Currents up to 1200 A (now 2400 A).
- **4,000 IV curves per day.**

Public wire  $I_c$  database <https://www.robinson.ac.nz/hts-wire-database>



# Robinson public wire $I_c$ database

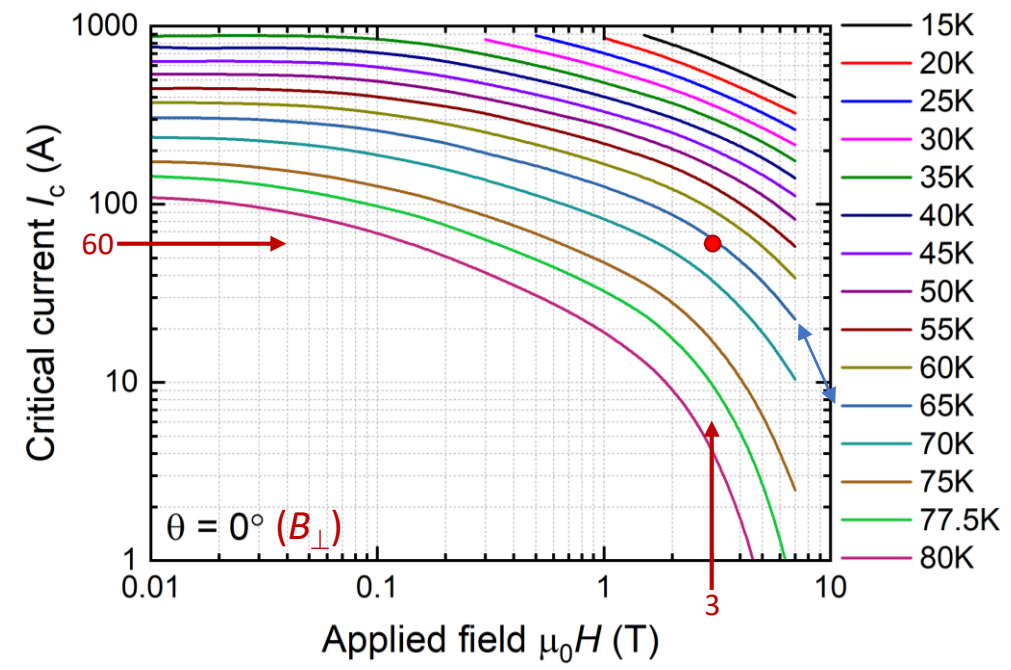
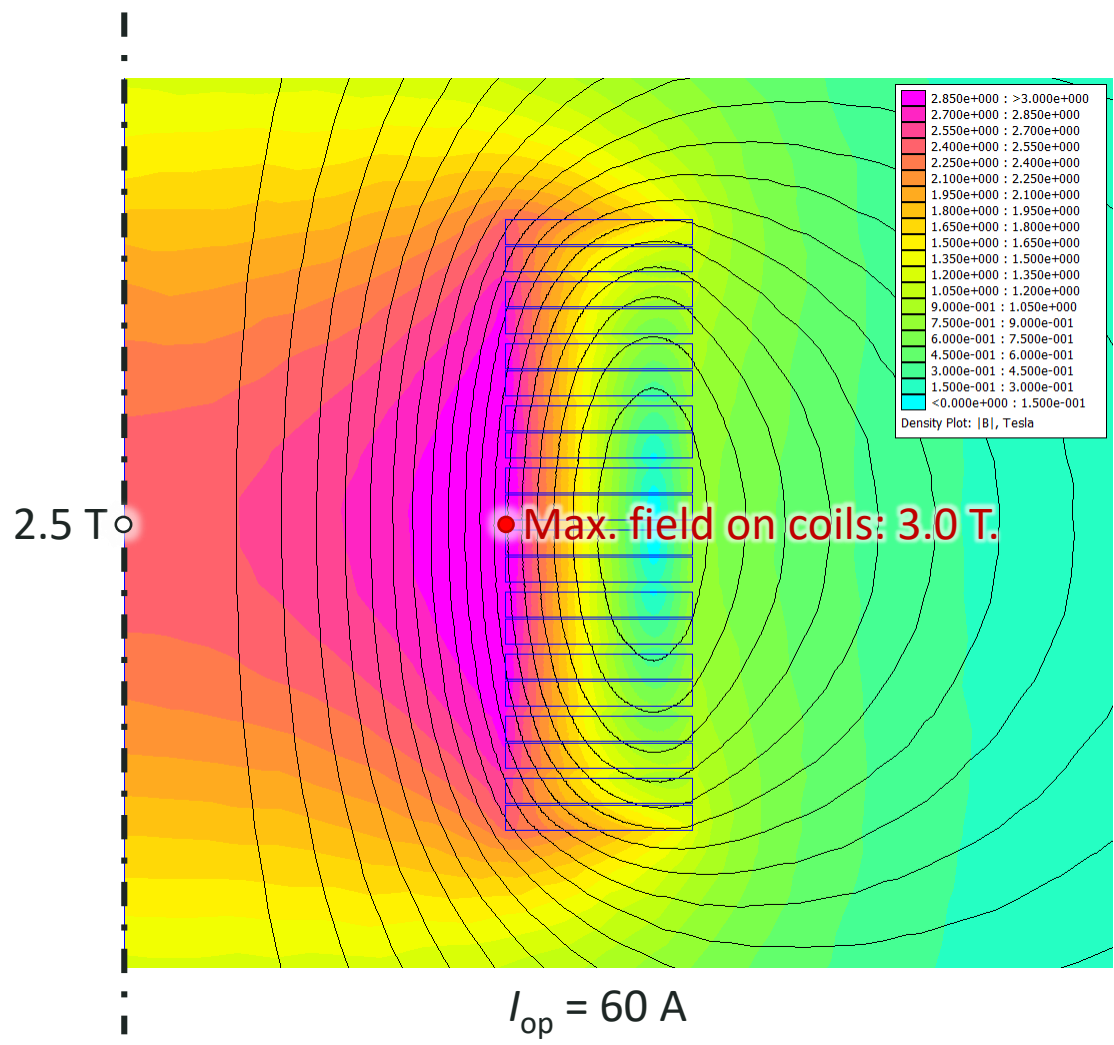
S. C. Wimbush and N. M. Strickland.  
A public database of high-temperature superconductor critical current data.  
*IEEE Trans. Appl. Supercond.* **27**, 8000105 (2017).

<https://www.robinson.ac.nz/hts-wire-database>

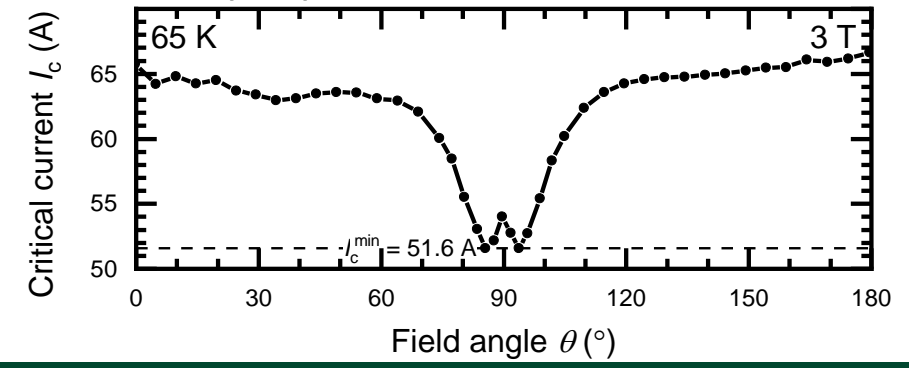
The image displays the Robinson public wire  $I_c$  database interface. On the left, a list of datasets is shown, with 'Shanghai Superconductor PA1212 2G HTS' highlighted in red. The main area features a plot of critical current  $I_c$  (A) versus magnetic field (T) for various temperatures, with the 77.5K data series highlighted in red. Below the plot, a list of files for different temperatures is shown, with '77.5K angle dependences.xlsx' and 'IV curves.zip' highlighted in red. On the right, a detailed view of the 'Shanghai Superconductor PA1212 2G HTS' dataset is shown, including a table of critical current data and a description of the dataset.

	A	B	C	D	E	F	G	H	I
1	Temperature (K)	Field (T)	Angle (°)	$I_{c/w}$ (A/cm)	$I_c$ (A)	$n$	$V_0$ ( $\mu$ V)	$V_1$ ( $\mu$ V/A)	Hall field (T)
2	77.48	0	0	362.24	144.9	27.18	0.01192	-0.00004	-0.001
3	77.52	0	5	362.72	145.09	27.35	0.02302	0.00001	-0.001
4	77.51	0	10	363.23	145.29	27.25	0.03728	0.00004	-0.001
5	77.5	0	15	364.13	145.65	28.11	0.07432	0.00011	-0.001
6	77.5	0	20	364.06	145.63	27.82	0.0241	0.00031	-0.001
7	77.51	0	25	364.68	145.87	27.72	0.04488	0.00019	0
8	77.5	0	30	364.92	145.97	27.7	0.05197	0.00029	-0.001
9	77.5	0	35	365.41	146.16	28.08	0.07512	0.00003	-0.001
10	77.5	0	40	365	146	27.61	0.06295	0.00016	0.001
11	77.5	0	45	365.16	146.07	28.02	0.06258	0.00016	-0.001
12	77.5	-0.001	50	365.2	146.08	28.31	0.02087	0.00026	-0.001
13	77.5	0	55	365.2	146.08	28.24	0.01767	0.00016	0.001
14	77.5	0	60	364.82	145.93	27.83	0.03976	0.00006	0.001
15	77.5	0	65	365	146	27.94	0.05844	-0.00007	0.001
16	77.5	0	70	364.84	145.94	27.96	0.0389	0.00006	0.001

Central field target: 2.5 T.

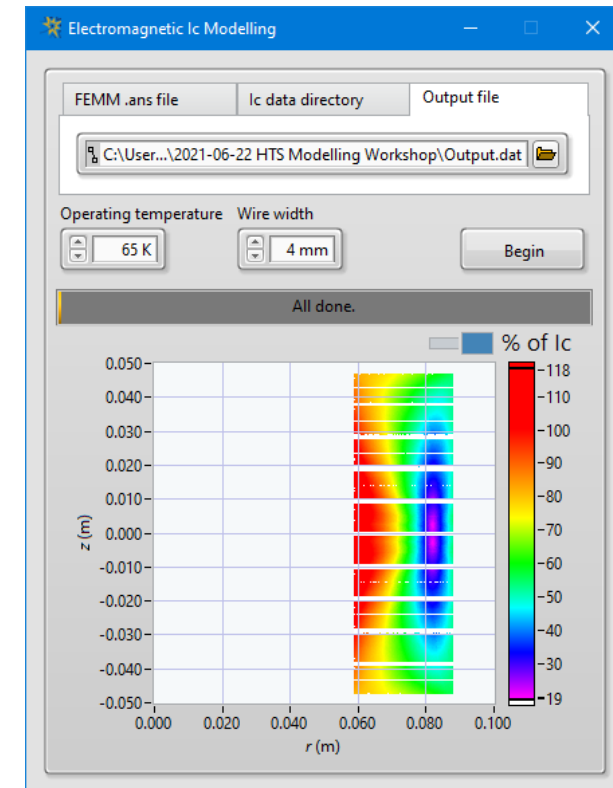


Operating temperature  $< 65 \text{ K}$ .  
 $0^\circ$  (field perpendicular) is **not** minimum  $I_c$ !



# Utilise full angle-dependent $I_c$ dataset

- Export  $(B, \theta)$  values at each element in the mesh.
  - (In FEMM, you need to process the potentials to give  $\mathbf{B}$ . Other packages may provide a direct export.)
  - For the 2D axisymmetric case, the components are  $B_r$  ( $B_{\perp}$ ) and  $B_z$  ( $B_{\parallel}$ ), which is very convenient.
  - In 3D, need to process the three components of  $\mathbf{B}$ , neglecting any in-plane variation in  $I_c$ .
- For a given operating temperature, we then have a  $\{T, B, \theta\}$  triplet at each element of the mesh that can be used to lookup an interpolated  $I_c(T, B, \theta)$  table to yield a local  $I_c$  value at each mesh element within the conductor.
- The operating current  $I_{op}$  as a percentage of this local  $I_c$  tells us what fraction of  $I_c$  we are operating each point in the coil at.
- A utility to perform this process for any FEMM model and SuperCurrent  $I_c$  dataset is available at <https://github.com/scwimbush/Electromagnetic-Ic-Modelling>.



# Interpolation of $I_c(T, B, \vartheta)$ datasets

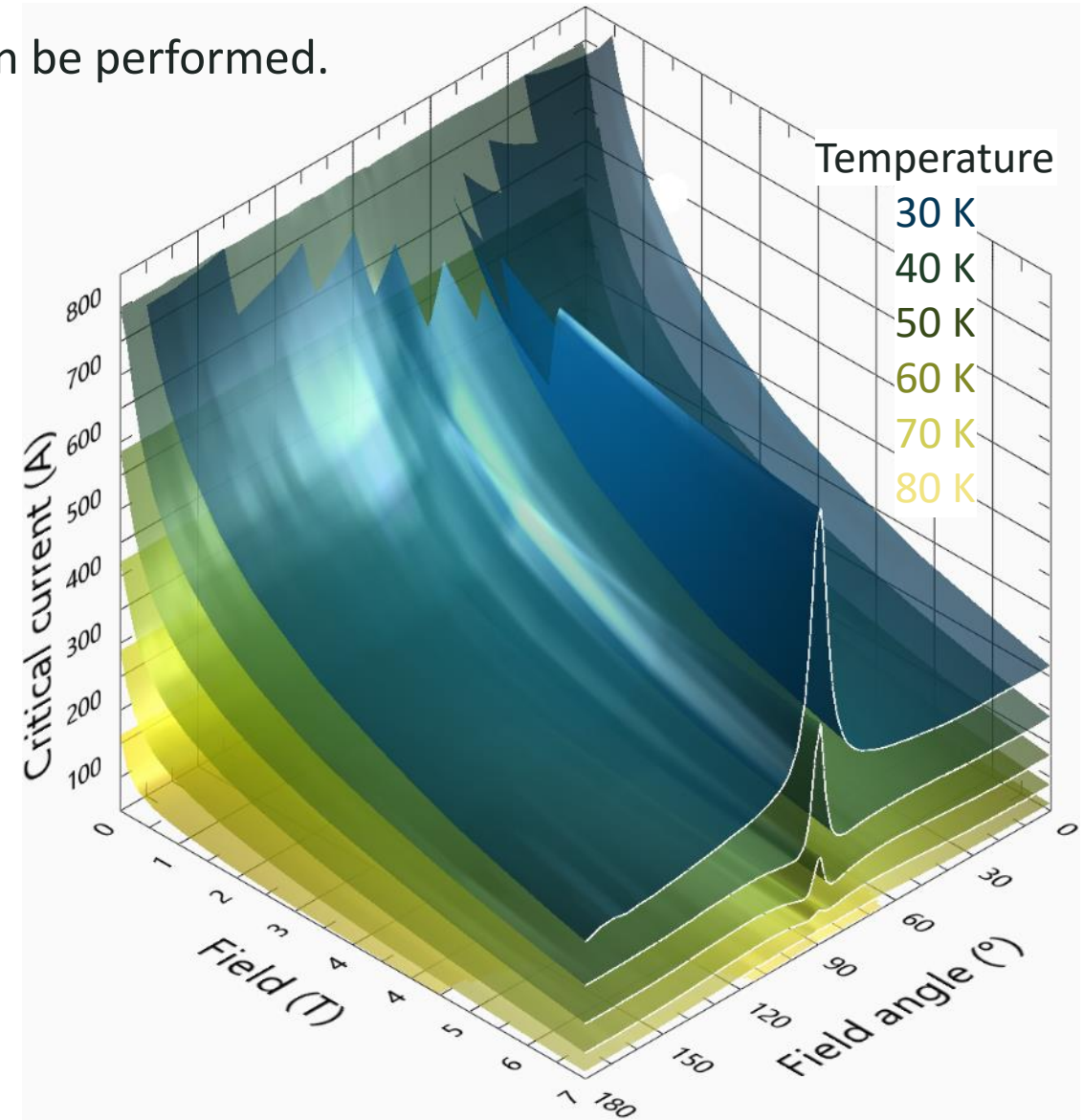
With datasets of our density, extremely good interpolations can be performed.

Simple point-to-point interpolations, with a few tricks:

- First interpolate the angle dependences – smoothly varying.
- Then at each interpolated angle:
  - Interpolate the field dependences *logarithmically*.
  - Interpolate the temperature dependences linearly.

Doing these interpolations is the slowest part of the analysis.

Presently strictly an **interpolation**;  
**extrapolation** is challenging to perform robustly and reliably.



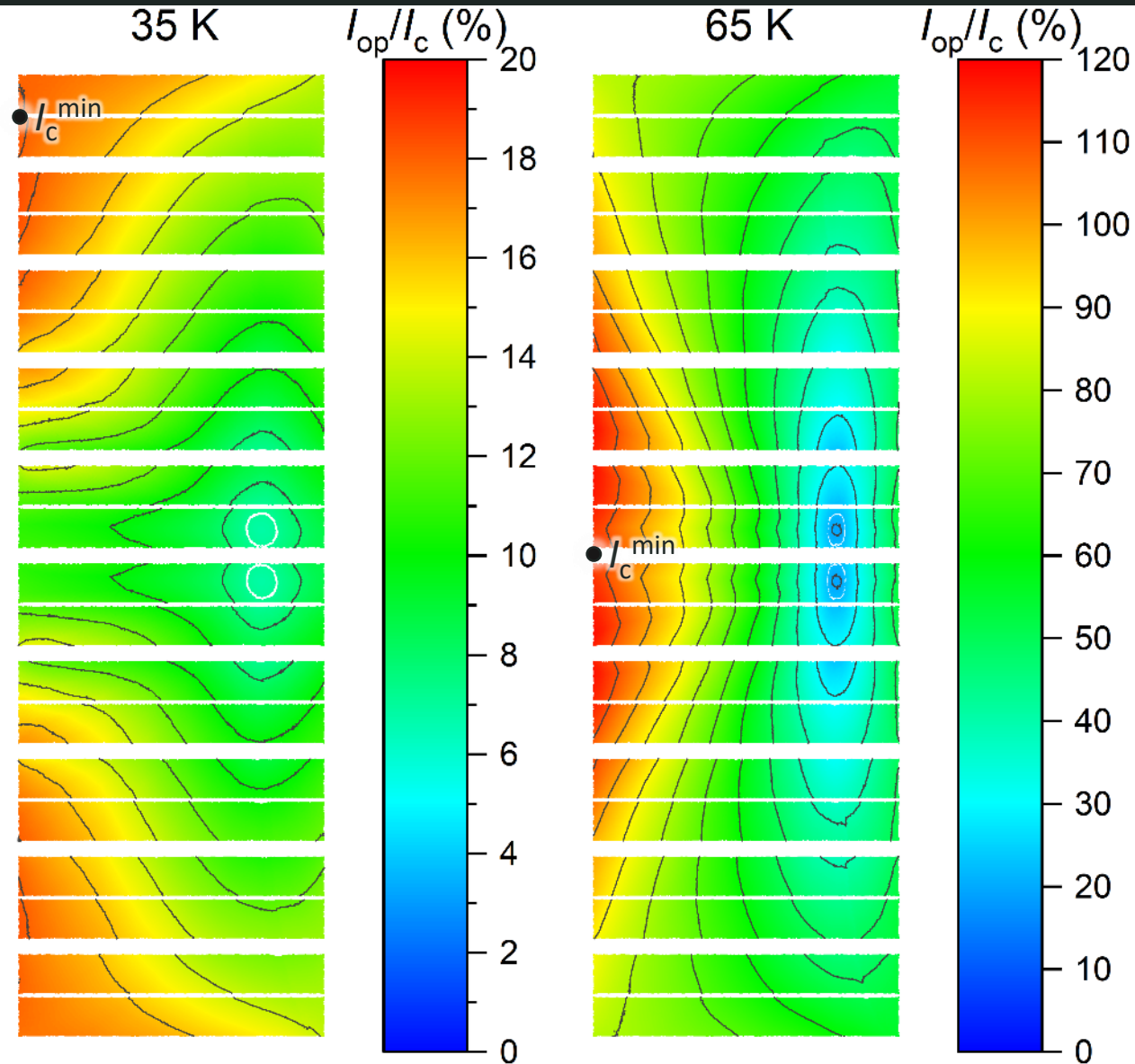
# Results of $I_c$ lookup

Looking at the  $I_c$  map across the conductor at our first proposed operating temperature of 65 K, we see:

- The critical point on the coils is the high field (fully in-plane!) region at the centre of the coil pack.
- We are 20% short of the performance required to operate.

Refining the analysis at different temperatures shows we could expect to operate at 62 K, approximately as predicted by the (true) minimum  $I_c$  analysis. (This is the case because the field angle at the critical point coincides with the angle of minimum  $I_c$ .)

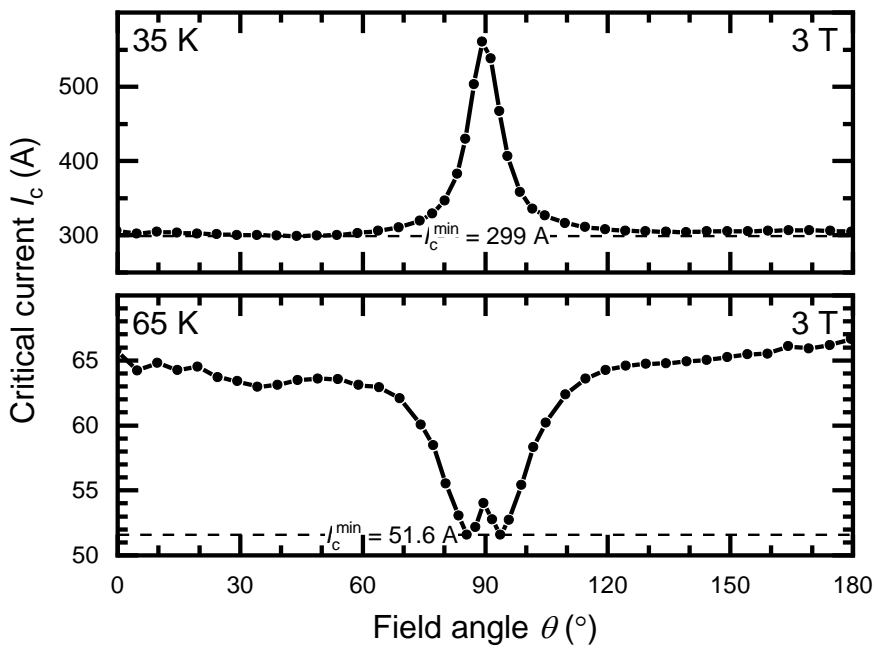
If we drop the operating temperature to 35 K, the critical point shifts to the more commonly observed inner edge of the end coils, where a moderate field strength and an unfavourable field direction combine. Here a minimum  $I_c$  analysis would underestimate the available  $I_c$ .



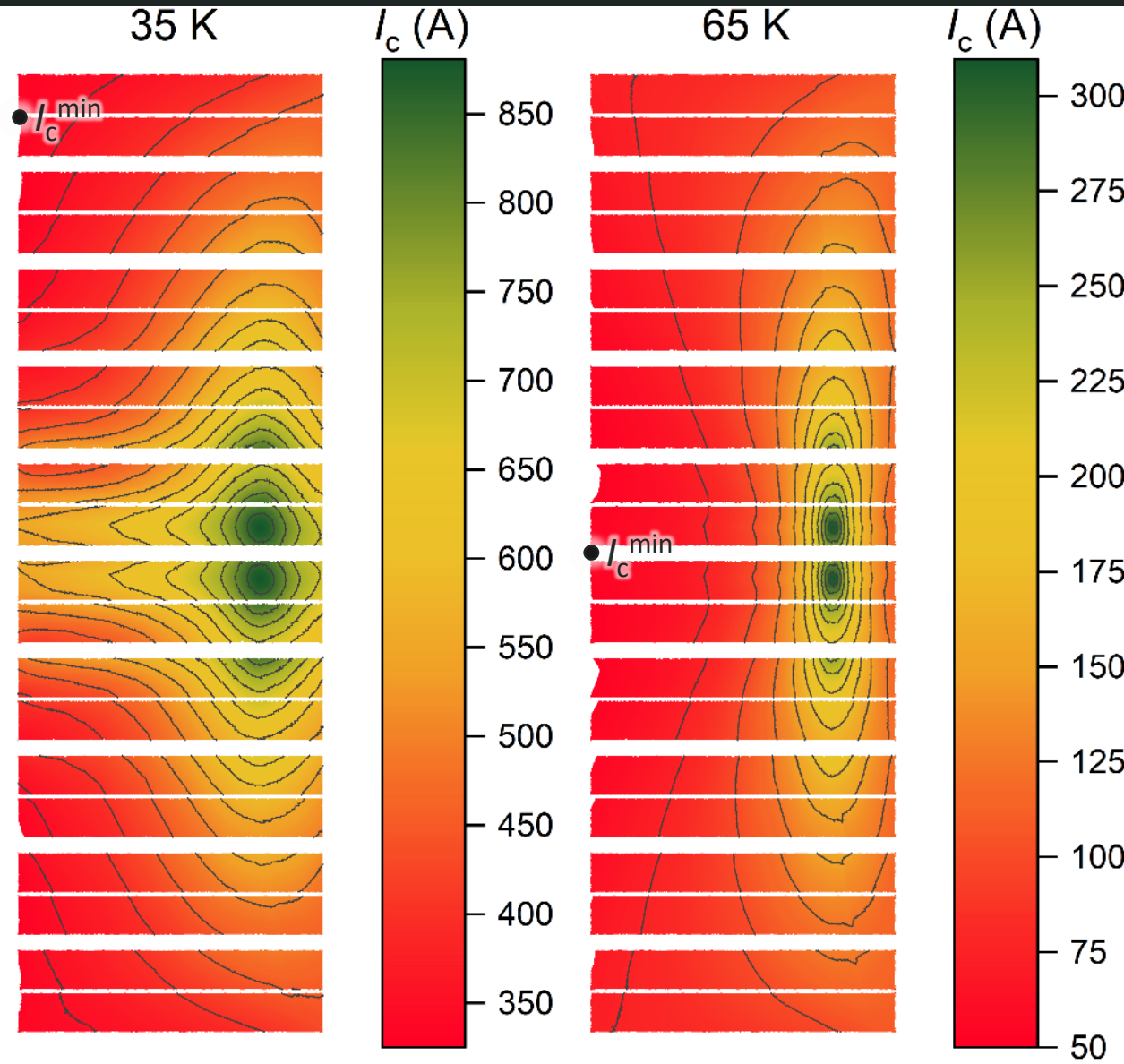


# Results of $I_c$ lookup

The reason for the shift in position of the critical point with temperature is evident upon comparison of the angle dependence of  $I_c$  under the different conditions.



This aspect of real wire behaviour cannot be captured by  $I_c(B_{||}, B_{\perp})$  field dependences alone.



# Applications

# Hybrid windings

Now we know exactly where in the coil pack the critical region occurs, we can replace selected coils with higher performance wire, or simply stack the coils we have on hand in an appropriate order.

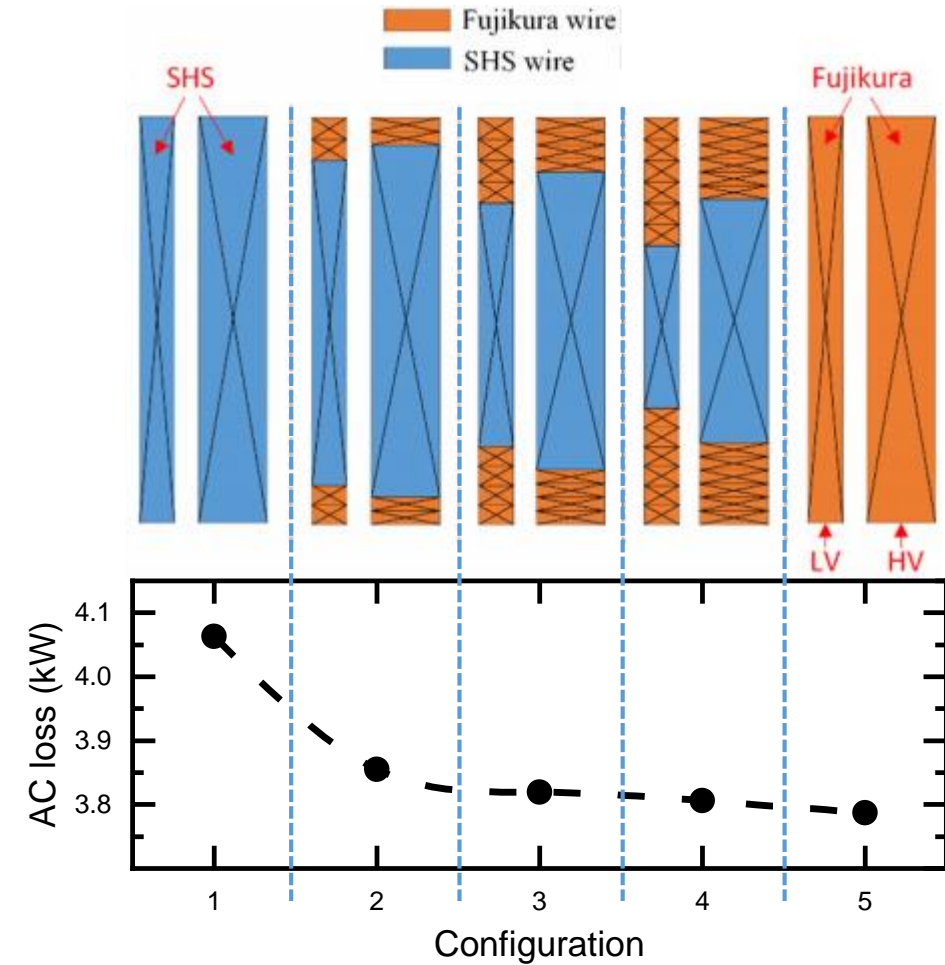
In the example presented so far, at 65 K:

- End coils  $I_{op}/I_c = 90\%$ .
- Mid coils  $I_{op}/I_c = 120\%$ . → Substitute better wire for these coils (only).

Many manufacturers provide wire with different performance specifications or we can select the most appropriate wire from multiple manufacturers.

This extends beyond operating current to other performance metrics.

In the real-world example of our traction transformer design, we can lower the overall ac loss by 5–10% by incorporating relatively small quantities of high-performance wire in the right places.



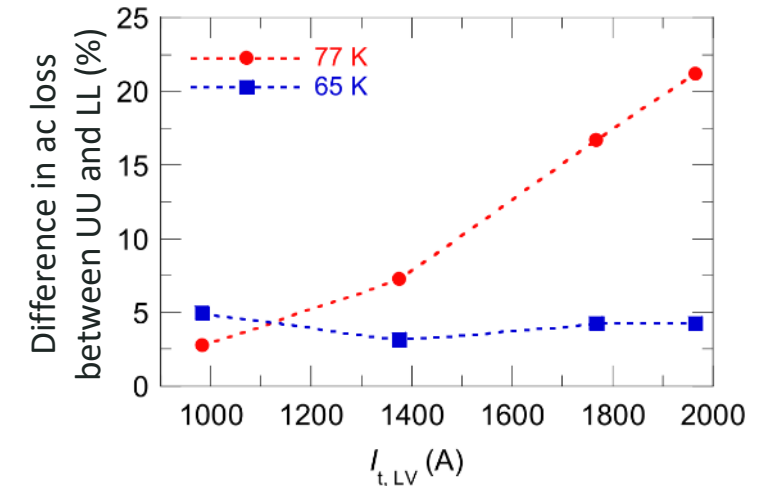
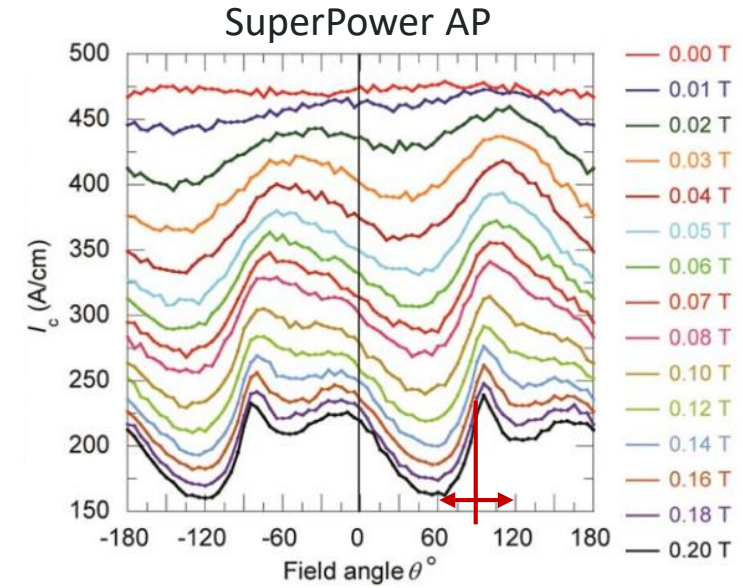
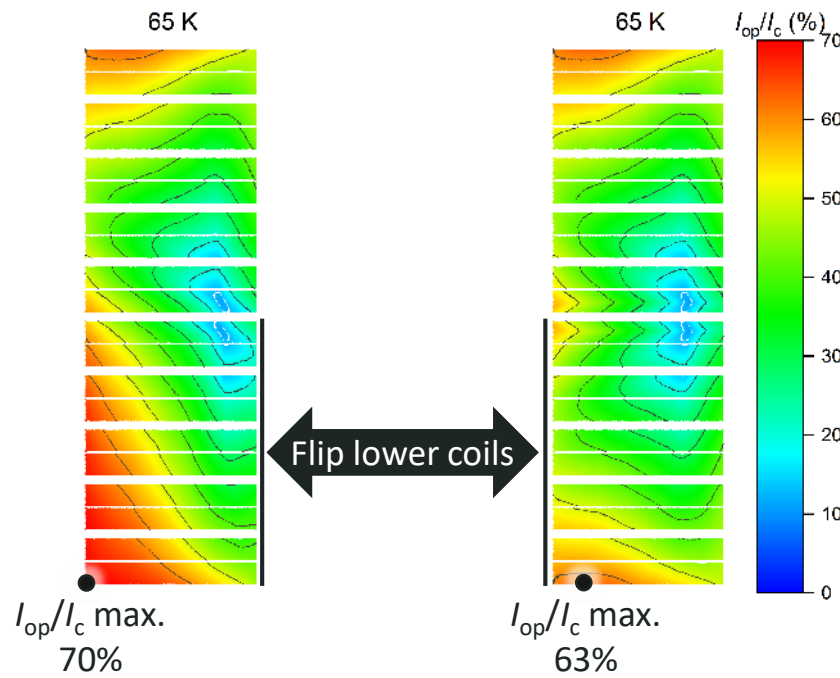
# Flipped coils

Z. Jiang, W. Song, X. Pei, J. Fang, R. A. Badcock and S. C. Wimbush.  
15% reduction in AC loss of a 3-phase 1 MVA HTS transformer by exploiting asymmetric conductor critical current.  
*J. Phys. Commun.* 5, 025003 (2021).

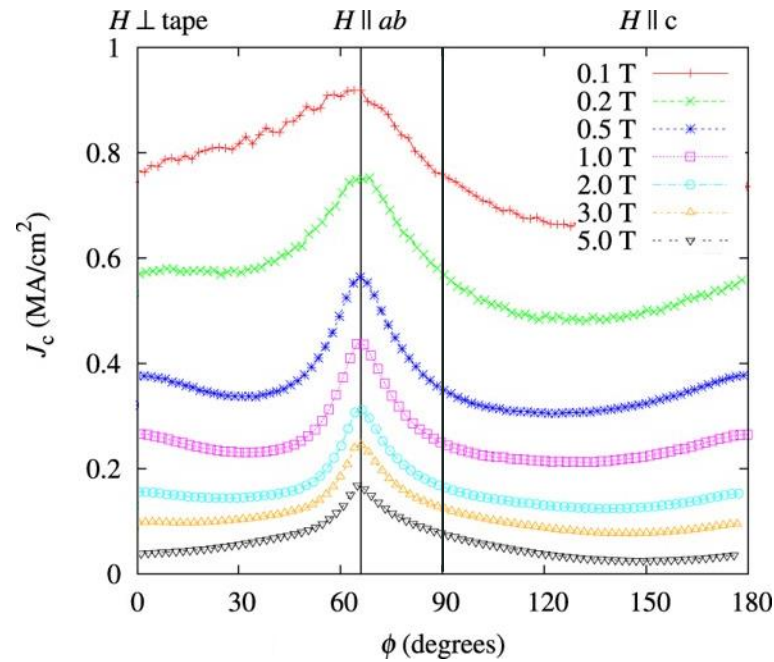
Now that we explicitly take account of the real anisotropy of the conductors, not an approximate functional form, we can exploit detailed characteristics such as asymmetry either side of the in-plane peak.

For some conductors, this is not strongly evident, but for some it is.

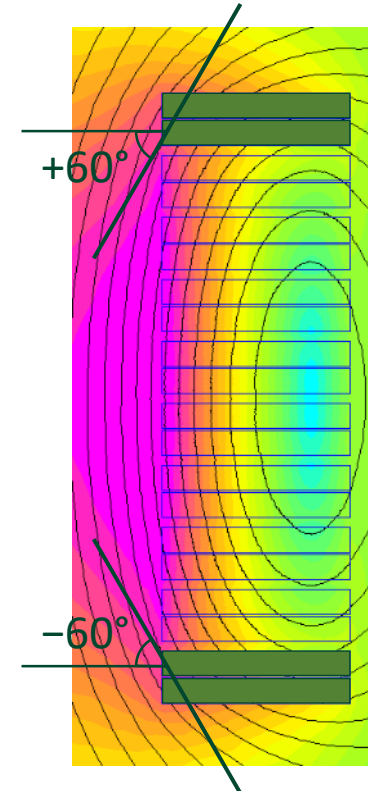
Taking advantage of this is as easy as ensuring the “correct” orientation of the coils when they are stacked.



Inherent asymmetry tends to be evident only at relatively low fields. But we can intentionally select a conductor (e.g. one produced by inclined substrate deposition) that is particularly appropriate to the required operating conditions. In this case, we must ensure correct orientation and we would also only utilise such a conductor in the relevant locations in the coil pack.



THEVA

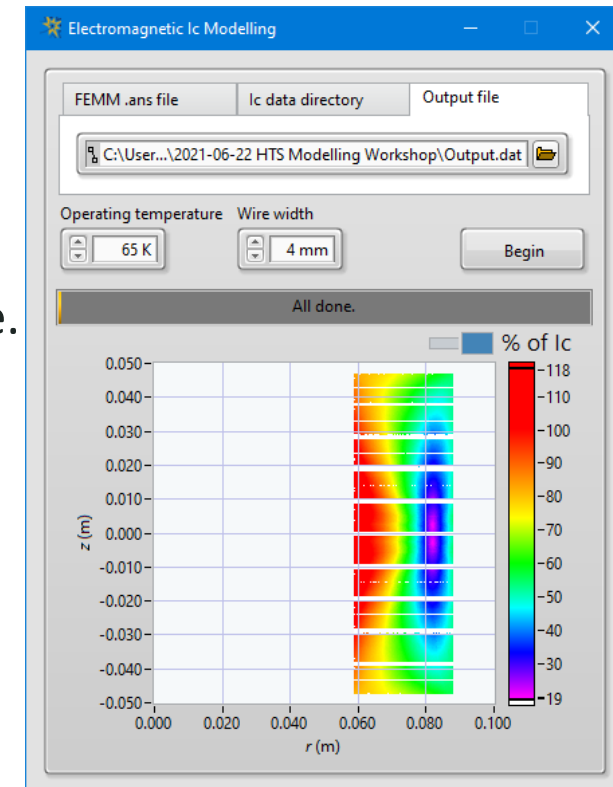


To our knowledge, no such demonstrator has yet been produced.

# Summary

# Summary

- Electromagnetic modelling utilising full angle-dependent  $I_c$  data is tractable.
- Exemplary  $I_c$  datasets are available to trial and refine techniques.
- Targeted data acquisition for specific projects is feasible.
  
- Such modelling reveals features of device design that could otherwise lead to failure.
- Optimisation of real-world devices offers a 10–20% enhancement in performance leading to real benefits.
  
- These analyses lead to novel design features such as:
  - Hybrid windings.
  - Flipped coils.
  - Inclined planarity conductors.



<https://www.robinson.ac.nz/hts-wire-database>

<https://github.com/scwimbush/Electromagnetic-Ic-Modelling>

Thank you for your attention!