

# Modelling of the pulsed field magnetization of a (RE)BaCuO bulk with a superconducting weld

**\*Rémi Dorget<sup>1,2</sup>, Kévin Berger<sup>1</sup>, Joseph Longji Dadiel<sup>3</sup>, Kimiaki Sudo<sup>3</sup>, Naomichi Sakai<sup>3</sup>, Tetsuo Oka<sup>3</sup>, Masato Murakami<sup>3</sup> and Jean Lévêque<sup>1</sup>**

<sup>1</sup> Université de Lorraine, GREEN, F-54000 Nancy, France

<sup>2</sup> Safran Tech, Electrical & Electronic Systems Research group, Rue des Jeunes Bois, Châteaufort, 78114 Magny-Les-Hameaux, France

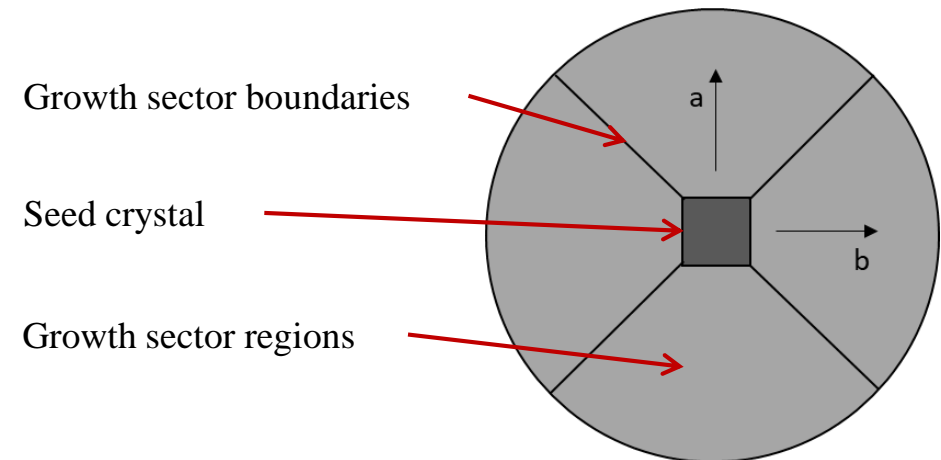
<sup>3</sup> Shibaura Institute of Technology ,3 Chome-7-5 Toyosu, Koto, Tokyo 135-8548 - Japan



- Top seeded melt growth
- RE-Ba-Cu-O bulk welding process
- Description of the model
- Results

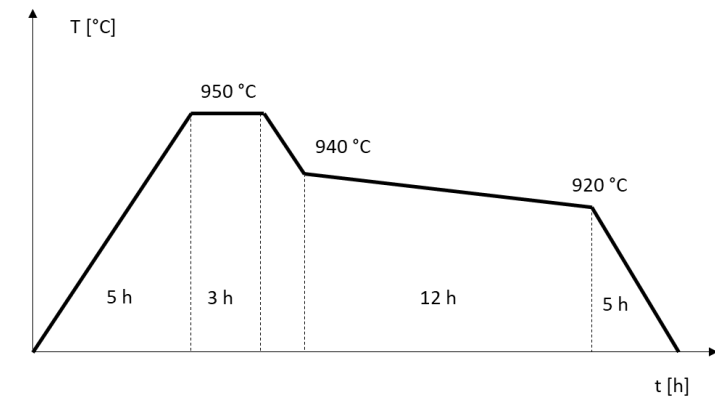
# Top seeded melt growth (TSMG)

- Pellet of RE-Ba-Cu-O pressed then melted and slowly cooled to let the crystal grow
- The seed crystal (RE-Ba-Cu-O with higher melting point) give the crystal orientation
  - ❖ Examples of seed crystals :  
Nd-Ba-Cu-O or Sm-Ba-Cu-O
- Several hours of oxygen annealing



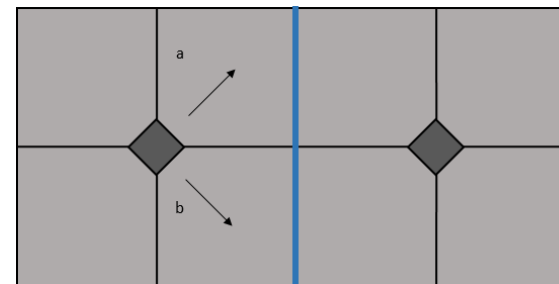
# Bulk welding process

- Solder material: RE-Ba-Cu-O with low melting point
- Process similar to TSMG: The solder material is melted while the bulk body act as the seed

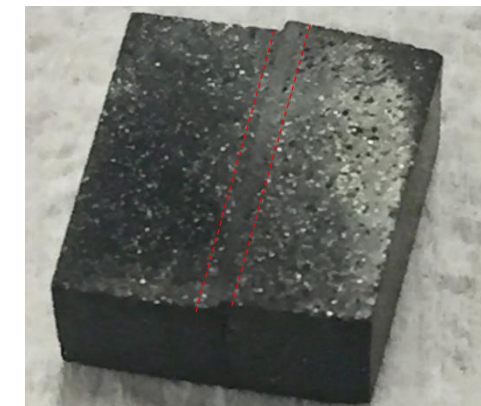


Example of the temperature process for joining Y-Ba-Cu-O + 10%Ag with Er-Ba-Cu-O + 10%Ag

Material	T <sub>p</sub> [°C]
Y-Ba-Cu-O	1008 °C
Er-Ba-Cu-O	980 °C
Y-Ba-Cu-O + 10%Ag	956 °C
Er-Ba-Cu-O + 10%Ag	937 °C

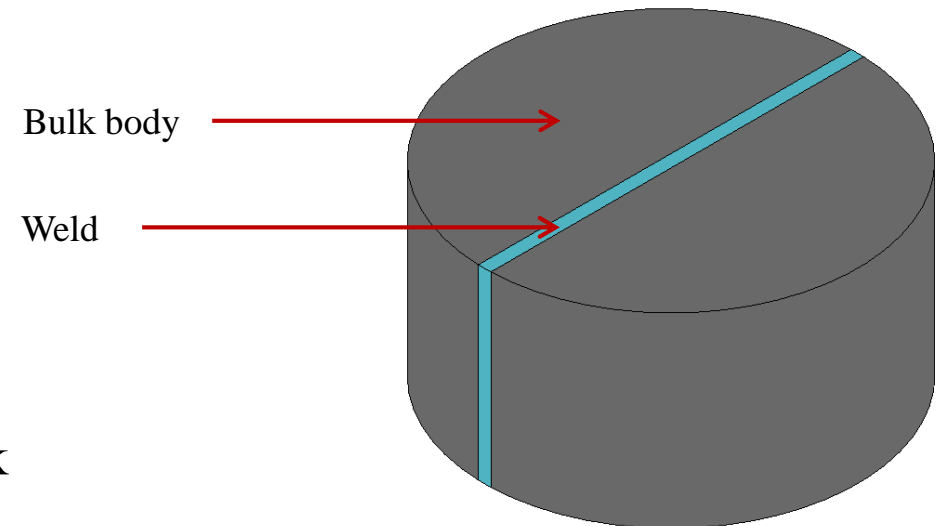


Good grain connection is obtain along the 110 plane



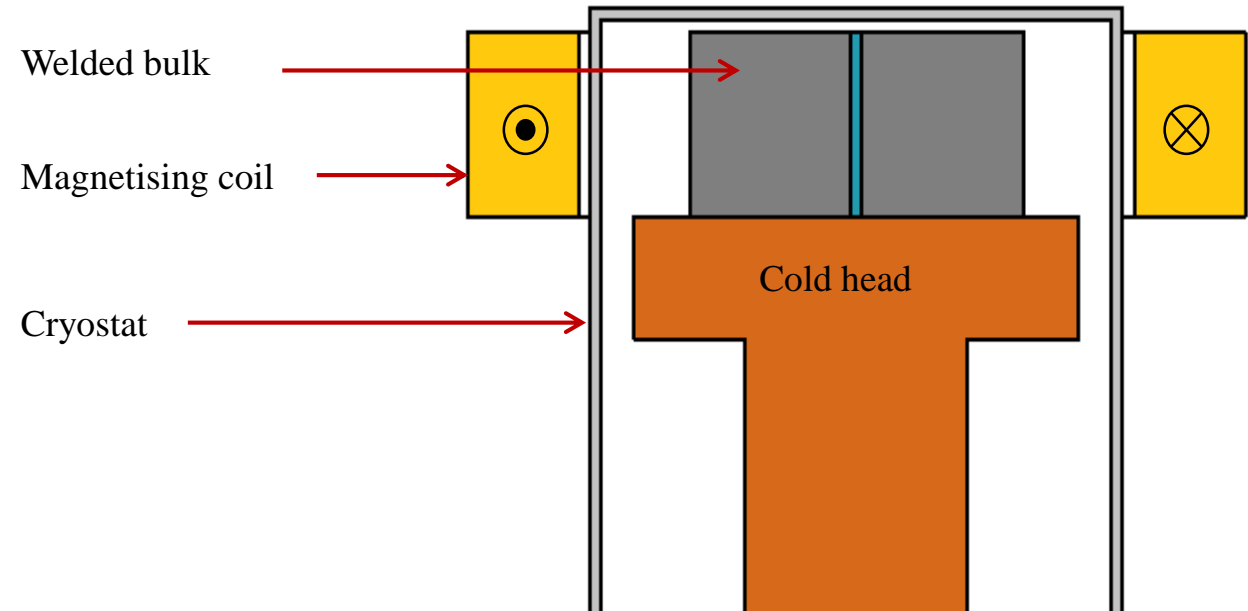
# Case study

- Simulation of the weld behavior during pulsed field magnetisation (PFM)
- Bulk body:
  - ❖ Radius : 30 mm
  - ❖ Height : 15 mm
  - ❖ Homogeneous superconducting properties
- Weld:
  - ❖ Thickness : 1 mm
  - ❖ Superconducting properties different from the bulk body
- Objective: study the magnetisation for different welds

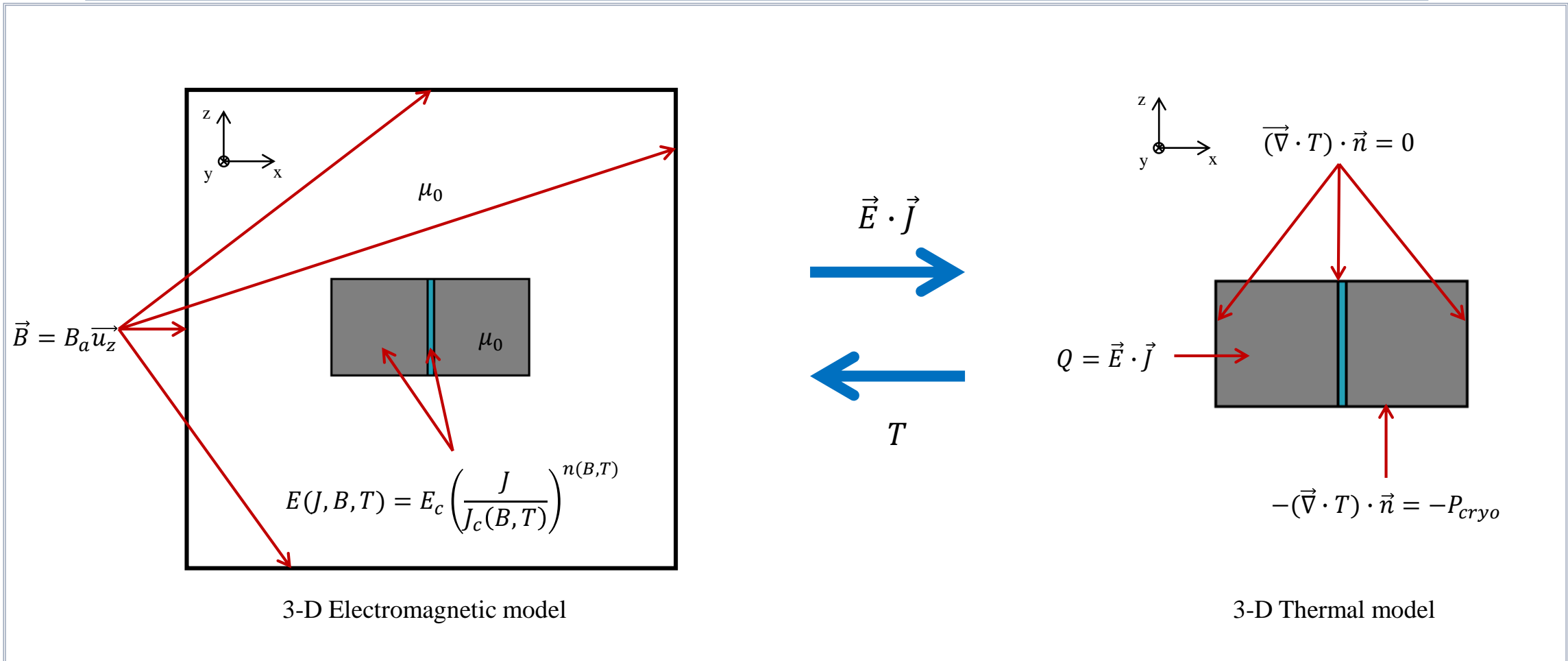


# Simulated setup

- Initial temperature :  
 $T_a = 60 \text{ K}$
- Cryocooler cooling power :  
 $P_{\text{cryo}} = 50 \text{ W}$
- Applied magnetic field :  
 $B_a = [0.5 \text{ T} : 9 \text{ T}]$



# Electromagnetic and thermal models



# Electromagnetic model



- H-formulation

- $J_c(B, T)$ :

- ❖ In the bulk body:
$$J_{c1}(B, T) = \frac{J_{c0}}{\left(1 + \frac{B}{B_0}\right)^\beta} \left(\frac{1 - T/T_c}{1 - T_0/T_c}\right)$$

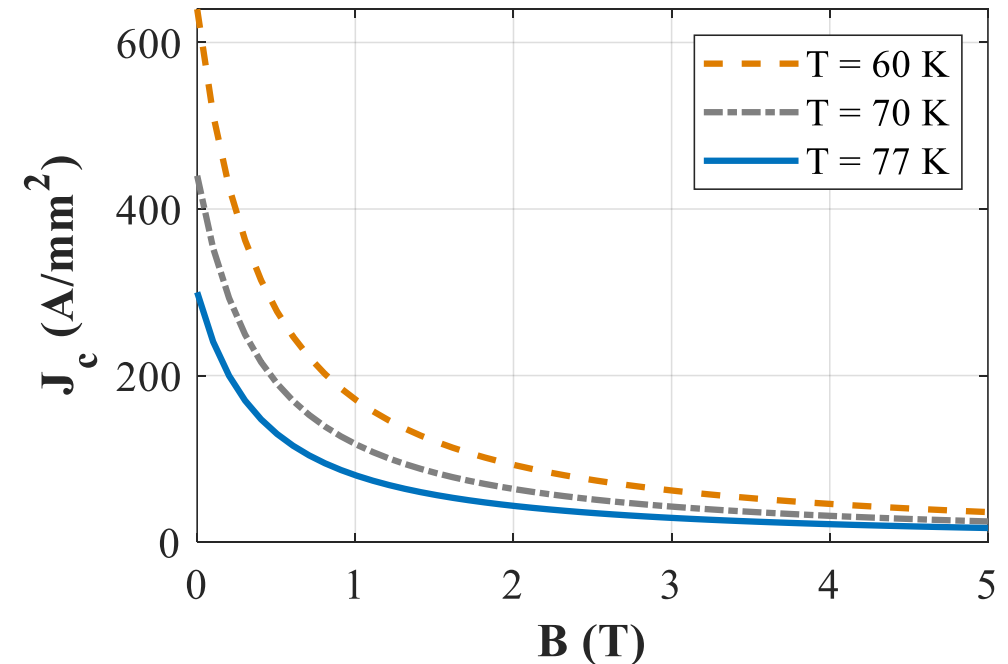
- ❖ In the weld:

$$J_{c2}(B, T) = \alpha J_{c1}(B, T)$$

- ❖ Weld to bulk body critical current ratio:

$$\alpha = [0.25 ; 0.5 ; 0.75 ; 1]$$

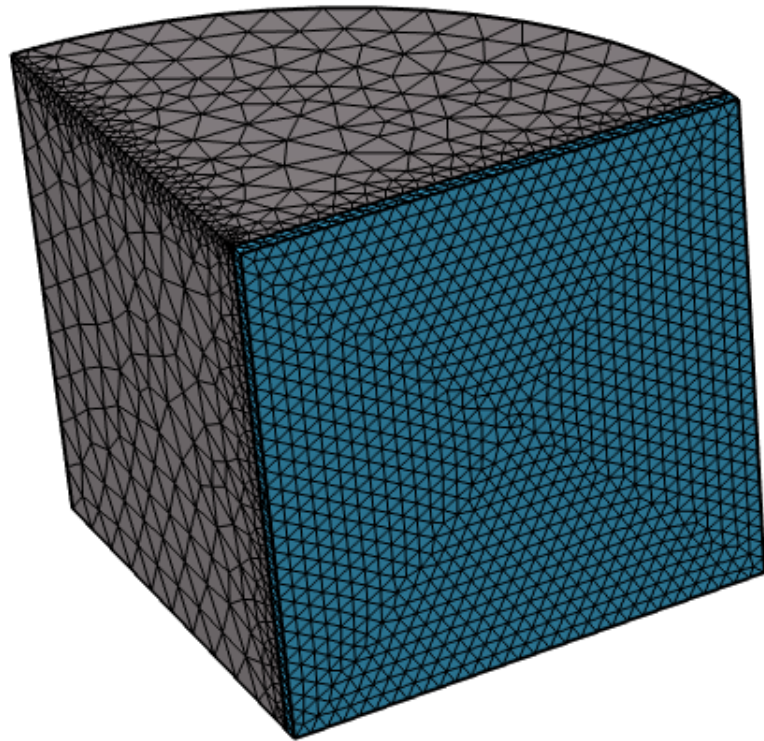
- $n(B, T) = \left(n_1 + \frac{n_0 - n_1}{1 + B/B_0}\right) \frac{T_0}{T}$





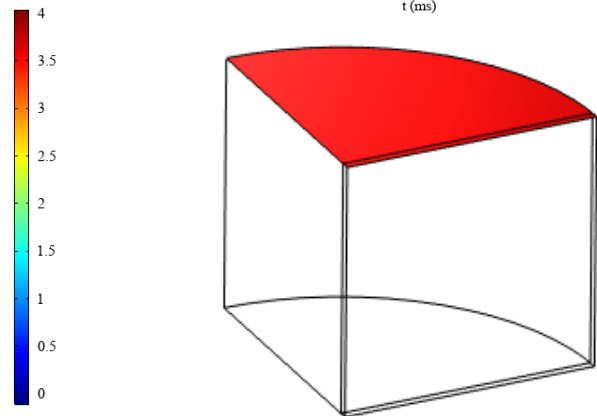
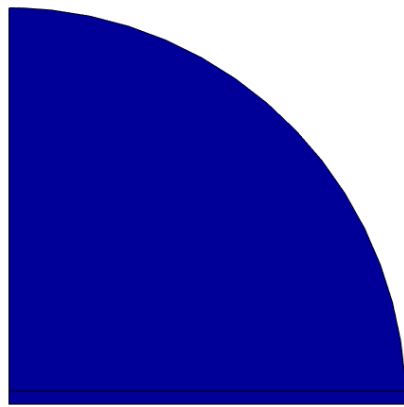
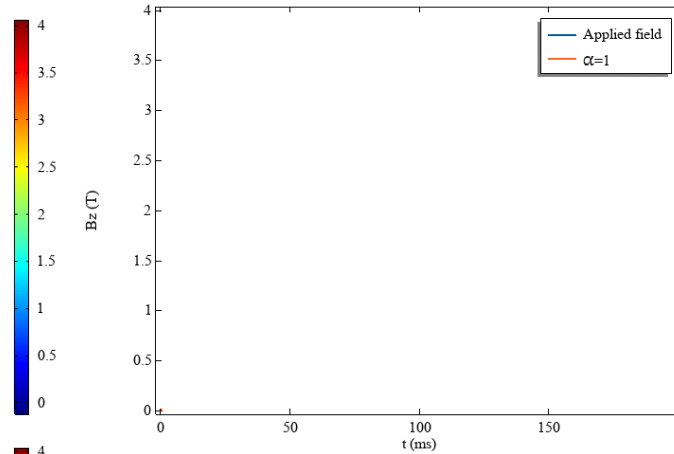
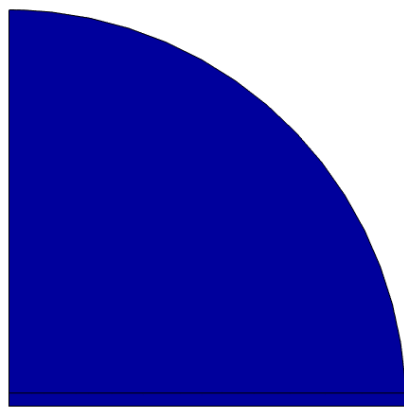
# Simulation parameters

- Due to symmetries  $\rightarrow$   $\frac{1}{4}$  of the geometry is simulated

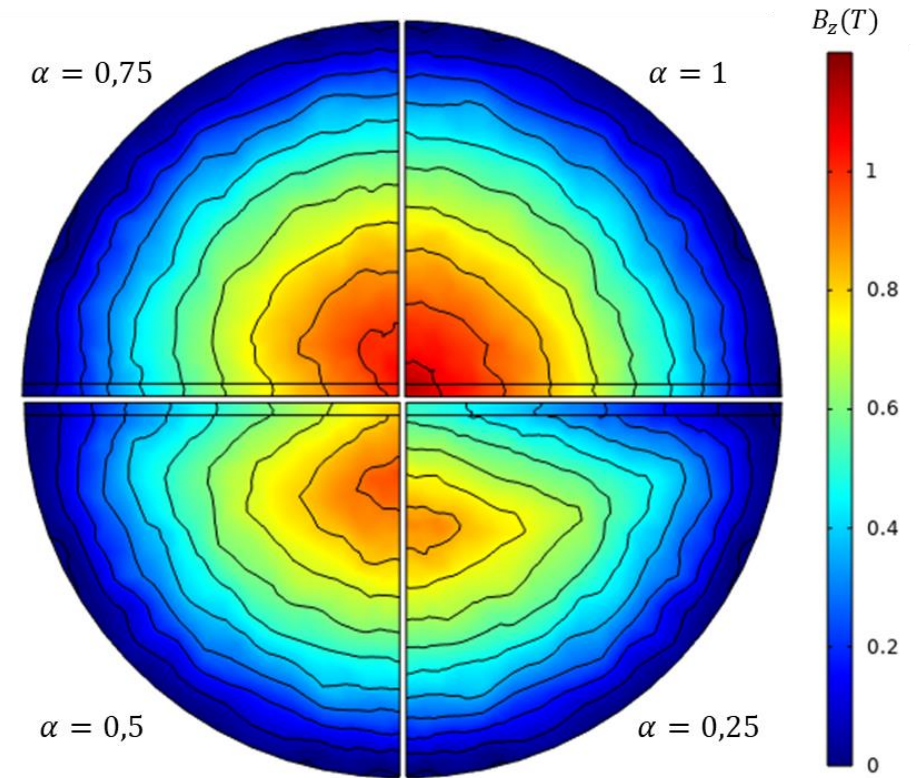


Parameter	Value	Description
$J_{c0}$	300 A/mm <sup>2</sup>	Self field critical current density at 77 K
$B_0$	0.5 T	Magnetic field dependance constant
$\beta$	1.2	Magnetic field dependance exponent
$n_0$	20	n exponent at 77 K and $B = 0$ T
$n_1$	6	n exponent at 77 K and $B \gg B_0$
$T_c$	92 K	Critical temperature
$T_0$	77 K	Reference temperature
$T_a$	60 K	Initial temperature
$B_a$	[0.5 T : 9 T]	Applied flux density
$\tau$	10 ms	Pulse time constant
$\alpha$	[0.25 : 1]	Weld to bulk body critical current ratio
$P_{cryo}$	50 W	Cooling power of the cold head
$d$	6 g/cm <sup>3</sup>	RE-Ba-Cu-O density
$C$	150 J/(kg.K)	Heat capacity
$\gamma$	5 W/(m.K)	Thermal conductivity

# Results – Field maps



Penetration of the magnetic field during a 4 T pulse  
Top:  $\alpha = 1$  Bottom :  $\alpha = 0.5$

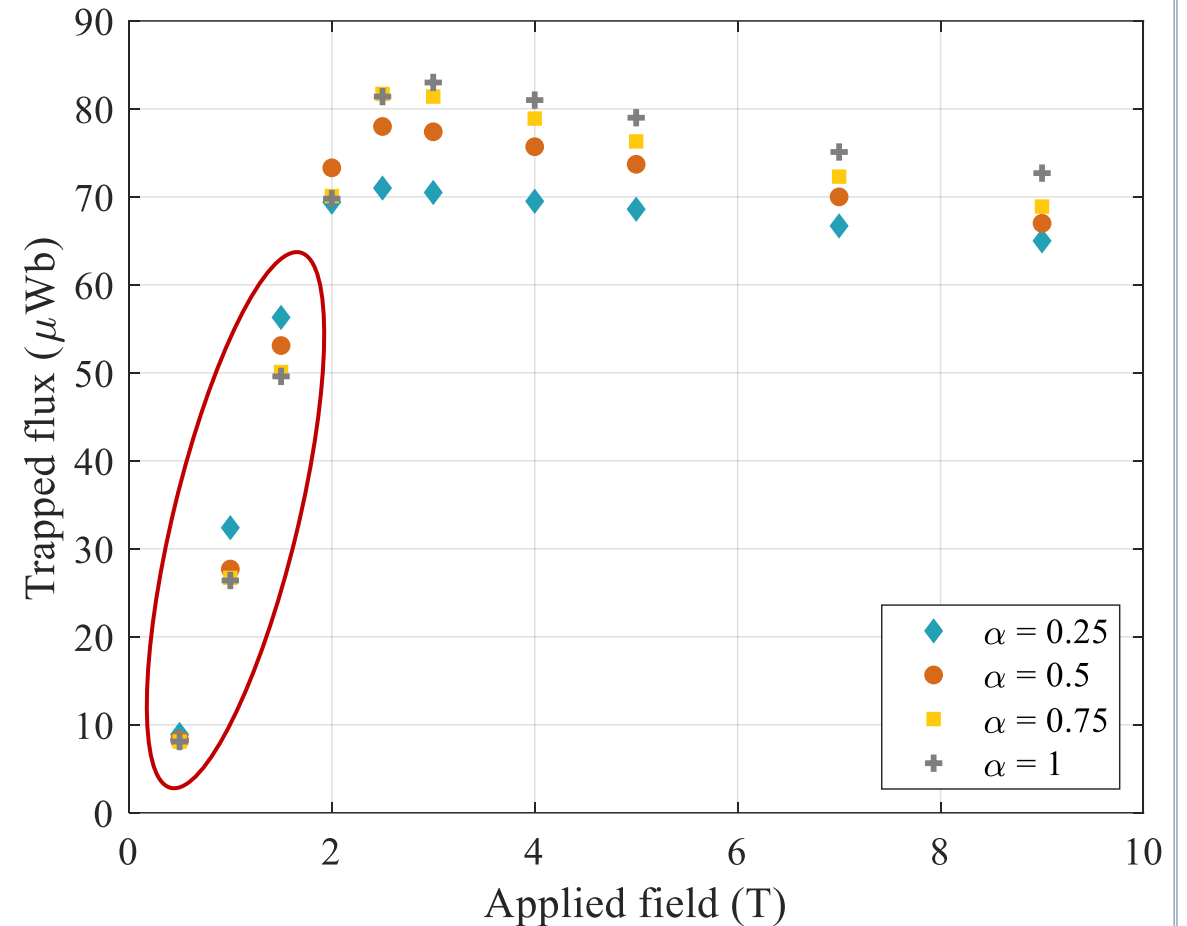


Trapped field map after 60 s

# Results – Trapped flux

Trapped flux on the bulk surface:

- Above 2 T → weld reduces the trapped flux
- Below 2 T → weld increases the trapped flux (up to 13 %)



# Conclusion



- A superconducting weld with a reduced critical current help the magnetic field to penetrate the bulk
  - ❖ Increased trapped flux at low applied field
  - ❖ Decreased trapped flux at high applied field
  - Applications with small inductor coil (magnetisation from armature windings)
- The solder can be doped to improve its thermal properties at the expense of the magnetic properties

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# Thank you for your attention

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Rémi Dorget, ☎ (+33) (0)6 82 52 22 86, ✉ e-mail: [remi.dorget@univ.lorraine.fr](mailto:remi.dorget@univ.lorraine.fr)