Fig. 3: Model of mechanical degradation of J<sub>c</sub> and *n* index accumulated from 1 to 8

Impregnated fiberglass separator



[1]: Hahn, S., Kim, K., Kim, K. et al. "45.5-tesla direct-current magnetic field generated with a high-temperature superconducting magnet". Nature 570, 496–499 (2019) [2]: E. Berrospe-Juarez et al. "Advanced electromagnetic modeling of large-scale high-temperature superconductor systems based on *H* and *T-A* formulations". SUST Vol. 4, No. 4, 2021



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**Abstract** – 2G HTS tapes are strong candidates for the development of future Spring boundary high magnetic field magnets. However, for such applications, the field stability and quality affected by the presence of large Screening Current-Induced Field (SCIF) and the mechanical degradation of the tape during the magnet operations are issues to be overcome for providing a reliable system for users of Pancake coil (PC) high magnetic field laboratories. A new model is proposed to simulate the magnetic and mechanical behavior of 2G HTS insert magnets under very high magnetic fields. This model includes the strong coupling between the electromagnetic and mechanical physics of REBCO tapes via the definition of their *n* index and critical current density *J<sub>c</sub>*. The case study is the Little Big Coil (LBC) which broke recently the record of the strongest continuous magnetic field achieved thus far.  $PC_{2}$ **Case study: Little Big Coil (LBC)**  $PC_1$ Record at **45.5 T** central field ,,,,,, Insert HTS magnet (Fig. 1): Roller boundary Fig. 2: Axisymmetric  $1/4$ <sup>th</sup> model of LBC • 4 mm width REBCO tapes Average *I<sub>c</sub>* at 77 K, 0.6 T: ~54 A  $J_{c,\varepsilon} = \sqrt{PF} \times GBM$ 12 racetrack coils • Background solenoidal field: 31 T function 2<sup>nd</sup> order polynomial Quench at 245 A Fig. 1: LBC [1]. **Strongly coupled mechanical and magnetic Model** Axisymmetric,  $1/4$ <sup>th</sup> of magnet cross-section  $\Rightarrow$  6 pancakes (see Fig. 2) Mechanics <>>
Magnetics • Current ramp rate: 0.068 A/s • Target field: 45 T • Electromagnetic model: homegeneous *T-A* formulation [2]  $\epsilon_{\rm irr,1}$   $\epsilon_{\rm irr,3}$ Mechanical model: elastoplastic (nonlinear  $\sigma$ - $\varepsilon$  curve)  $\epsilon = \epsilon_{\rm n}$ **Strong coupling** carried out by the critical current *J<sub>c</sub>* and the *n*  $n = n_r + (n_0 - n_r) \times GBMF$ index both depending on strain  $\varepsilon$  (see Fig. 3)  $n_{\ast}$ • Critical current depending on field magnitud and orientation  $n_0$  = n<sub>0</sub>(*B*)  $\simeq$  cst through the Kim relation Normalized  $J_{{\it c}0}$  $J_c(\mathsf{B}, \varepsilon) =$  $\overline{\alpha} * I_{c,\varepsilon}$  $^{2}_{\parallel}$  +  $B^{2}_{\perp}$ -  $1 + \frac{\gamma^2 B_{\parallel}^2}{\gamma}$ -  $B_0^2$ Two mechanical assumptions have been considered: 1) the tapes are glued together (bulk model), 2) Some block of tapes are radially free to move respectively to others (semi-free model)  $\epsilon_{\rm irr,1}$  $\epsilon_{\text{irr,3}}$ 

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# Impact of strain-dependent *J*<sub>c</sub> on SCIF in 2G HTS magnets

### Generalized bell-shaped Membership

Virgin curve (1-2-4-6-8):  $J_{c,e}^{vg}$ 1<sup>st</sup> degradation (3-2-4-6-8) :  $J_{c1,c}$  $2<sup>nd</sup>$  degradation (5-4-6-8):  $J_{c2,\epsilon}$  $3^{\text{rd}}$  degradation (7-6-8):  $J_{c3,e}$ 



Virgin curve  $(1-2-4-6-8)$ : *n* 1<sup>st</sup> degradation (3-4-6-8) :  $n_1$  $2<sup>nd</sup>$  degradation (5-6-8):  $n<sub>2</sub>$  $3<sup>rd</sup>$  degradation (7-6-8):  $n_3$ 



mechanical coupling